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TiAl-based intermetallic compound piston ring and process for treating the surfaces thereof

JP07083330

<ul style="list-style-type: none"> • Patent Assignee HONDA MOTOR • Inventor FUJIWARA YOSHIYA TOKUNE TOSHIO KANOYA IZURU • International Patent Classification C22C-014/00 C22C-019/00 C23C-014/00 C23C-014/02 C23C-014/06 C23C-014/32 F02F-005/00 F16J-009/26 • CPC Code C22C-019/00; C23C-014/00/21; C23C-014/06/41; F05C-2201/021; F05C-2201/0412; F16J-009/26 	<ul style="list-style-type: none"> • Publication Information JPH0783330 A 1995-03-28 [JP07083330] <li style="text-align: right;"> • Priority Details 1993JP-0231449 1993-09-17 1994JP-0035082 1994-03-04 																												
<ul style="list-style-type: none"> • Fampat family <table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 30%;">JPH0783330</td> <td style="width: 10%;">A</td> <td style="width: 20%;">1995-03-28</td> <td style="width: 40%;">[JP07083330]</td> </tr> <tr> <td>EP0645463</td> <td>A2</td> <td>1995-03-29</td> <td>[EP-645463]</td> </tr> <tr> <td>EP0645463</td> <td>A3</td> <td>1995-05-17</td> <td>[EP-645463]</td> </tr> <tr> <td>JPH07243020</td> <td>A</td> <td>1995-09-19</td> <td>[JP07243020]</td> </tr> <tr> <td>EP0645463</td> <td>B1</td> <td>1997-12-29</td> <td>[EP-645463]</td> </tr> <tr> <td>DE69407525</td> <td>D1</td> <td>1998-02-05</td> <td>[DE69407525]</td> </tr> <tr> <td>DE69407525</td> <td>T2</td> <td>1998-04-16</td> <td>[DE69407525]</td> </tr> </table>		JPH0783330	A	1995-03-28	[JP07083330]	EP0645463	A2	1995-03-29	[EP-645463]	EP0645463	A3	1995-05-17	[EP-645463]	JPH07243020	A	1995-09-19	[JP07243020]	EP0645463	B1	1997-12-29	[EP-645463]	DE69407525	D1	1998-02-05	[DE69407525]	DE69407525	T2	1998-04-16	[DE69407525]
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- **Abstract:**

(EP-645463)


A piston ring for an internal combustion engine is formed of a TiAl-based intermetallic compound having a volume fraction V_f of L10 type TiAl (γ -phase) in a range represented by $V_f \geq 30\%$. Such piston ring has a light weight, a high rigidity and a high limit of the number of revolutions (rpm) of the engine. The piston ring is subjected to a thermal treatment, preferably between about 500 DEG C and 900 DEG C, and then a thin film of titanium nitride, chromium nitride, titanium-aluminum nitride or the like is formed on the surfaces by a physical vapor deposition process, such as ion-plating.. <IMAGE>

Claims

(EP-645463)

1. A piston ring formed of a TiAl-based intermetallic compound having a volume fraction V_f of L10 type TiAl represented by $V_f \geq 30\%$.
2. A piston ring according to claim 1, wherein said volume fraction V_f of L10 type TiAl is in a range represented by $V_f \geq 40\%$.
3. A process for treating a surface of a piston ring made of a TiAl-based intermetallic compound, comprising a step of forming a thin film on a surface of the piston ring by a physical vapor deposition, wherein a residual strain in said piston ring is removed by subjecting said piston ring to a thermal treatment prior to the formation of the thin film by said physical vapor deposition.
4. A process for treating a surface of a piston ring made of a TiAl-based intermetallic compound according to claim 3, wherein a thermal treatment temperature T in said thermal treatment is set in a range represented by $500 \text{ DEG.C} \leq T \leq 900 \text{ DEG.C}$.
5. A process for treating a surface of a piston ring made of a TiAl-based intermetallic compound according to claim 3 or 4, wherein said physical vapor deposition is an ion-plating.
6. A process for treating a surface of a piston ring made of a TiAl-based intermetallic compound according to claim 3, or 4, wherein said thin film is formed of a nitride selected from the group consisting of titanium nitride, chromium nitride and titanium-aluminum nitride.
7. A process for treating a surface of a piston ring made of a TiAl-based intermetallic compound according to claim 5, wherein said thin film is formed of a nitride selected from the group consisting of titanium nitride, chromium nitride and titanium-aluminum nitride.
8. A piston ring according to claim 1 or 2, wherein said TiAl-based intermetallic compound is substantially $\text{Ti}_{49.6} \text{Al}_{14.5} \text{V}_2 \text{Nb}_2 \text{B}_{1.4}$.
9. A piston ring according to the process of claim 3 or 4, wherein said TiAl-based intermetallic compound is $\text{Ti}_{49.6} \text{Al}_{14.5} \text{V}_2 \text{Nb}_2 \text{B}_{1.4}$.
10. A piston ring formed of a TiAl-based intermetallic compound having a volume fraction V_f of L10 type TiAl represented by $V_f \geq 30\%$ and having a thin film formed on a surface of the piston ring by a physical vapor deposition, wherein said piston ring is subjected to a thermal treatment prior to the formation of said thin film for removing a residual strain in said piston ring.
11. A piston ring according to claim 10, wherein a thermal treatment temperature T in said thermal treatment is set in a range represented by $500 \text{ DEG.C} \leq T \leq 900 \text{ DEG.C}$.
12. A piston ring according to claim 10 or 11, wherein said physical vapor deposition is an ion-plating.
13. A piston ring according to claim 10 or 11, wherein said thin film is formed of a nitride selected from the group consisting of titanium nitride, chromium nitride and titanium-aluminum nitride.

High strength and high ductility TiAl-based intermetallic compound EP-634496

<ul style="list-style-type: none"> • Patent Assignee HONDA MOTOR • Inventor FUJIWARA YOSHIYA TOKUNE TOSHIO • International Patent Classification C22C-014/00 • US Patent Classification PCLO=420420000 PCLX=420418000 • CPC Code C22C-014/00 	<ul style="list-style-type: none"> • Publication Information EP0634496 A1 1995-01-18 [EP-634496] <div style="text-align: right; margin-top: 5px;">  </div> <ul style="list-style-type: none"> • Priority Details 1993JP-0174476 1993-07-14 1993JP-0311547 1993-12-13 																												
<ul style="list-style-type: none"> • Fampat family <table style="width: 100%; border-collapse: collapse; margin-top: 5px;"> <tr> <td style="width: 30%;">EP0634496</td> <td style="width: 20%;">A1</td> <td style="width: 20%;">1995-01-18</td> <td style="width: 30%;">[EP-634496]</td> </tr> <tr> <td>JPH0776745</td> <td>A</td> <td>1995-03-20</td> <td>[JP07076745]</td> </tr> <tr> <td>US5514333</td> <td>A</td> <td>1996-05-07</td> <td>[US5514333]</td> </tr> <tr> <td>EP0634496</td> <td>B1</td> <td>1997-11-05</td> <td>[EP-634496]</td> </tr> <tr> <td>DE69406602</td> <td>D1</td> <td>1997-12-11</td> <td>[DE69406602]</td> </tr> <tr> <td>DE69406602</td> <td>T2</td> <td>1998-03-26</td> <td>[DE69406602]</td> </tr> <tr> <td>JP3626507</td> <td>B2</td> <td>2005-03-09</td> <td>[JP3626507]</td> </tr> </table> 		EP0634496	A1	1995-01-18	[EP-634496]	JPH0776745	A	1995-03-20	[JP07076745]	US5514333	A	1996-05-07	[US5514333]	EP0634496	B1	1997-11-05	[EP-634496]	DE69406602	D1	1997-12-11	[DE69406602]	DE69406602	T2	1998-03-26	[DE69406602]	JP3626507	B2	2005-03-09	[JP3626507]
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JP3626507	B2	2005-03-09	[JP3626507]																										

- **Abstract:**

(EP-634496)

A high strength and high ductility TiAl-based intermetallic compound includes a content of aluminum in a range represented by 42.0 atom % \leq A1 \leq 50.0 atom %, a content of vanadium in a range represented by 1.0 atom % \leq V \leq 3.0 atom %, a content of niobium in a range represented by 1.0 atom % \leq Nb \leq 10.0 atom %, a content of boron in a range represented by 0.03 atom % \leq B \leq 2.2 atom %, and the balance of titanium and unavoidable impurities. A product of the TiAl-based intermetallic compound is formed by only casting or casting followed by a homogenizing thermal treatment.

<IMAGE>

Claims

(EP-634496)

1. A high strength and high ductility of TiAl-based intermetallic compound comprising a content of aluminum (Al) in a range represented by $42.0 \text{ atom } \% \leq Al \leq 50.0 \text{ atom } \%$, a content of vanadium (V) in a range represented by $1.0 \text{ atom } \% \leq V \leq 3.0 \text{ atom } \%$, a content of niobium (Nb) in a range represented by $1.0 \text{ atom } \% \leq Nb \leq 10.0 \text{ atom } \%$, a content of boron (B) in a range represented by $0.03 \text{ atom } \% \leq B \leq 2.2 \text{ atom } \%$, and the balance of titanium and unavoidable impurities.
2. A high strength and high ductility TiAl-based intermetallic compound according to claim 1, wherein the main phase is an L10 type gamma phase, a ratio c/a between both lattice constants "a" and "c" in the crystal structure of said L10 type gamma phase being in a range represented by $c/a \leq 1.015$.
3. A high strength and high ductility TiAl-based intermetallic compound according to claim 2, wherein relationship between both lattice constants is $c/a > 1.0$.
4. A high strength and high ductility TiAl-based intermetallic compound according to claim 1, wherein the main phase is an L10 type gamma phase having a volume fraction percent equal to or greater than 80%.
5. A method for producing a high strength and high ductility TiAl-based intermetallic compound, comprising the steps of:
preparing a blank which includes a content of aluminum (Al) in a range represented by $42.0 \text{ atom } \% \leq Al \leq 50.0 \text{ atom } \%$, a content of vanadium (V) in a range represented by $1.0 \text{ atom } \% \leq V \leq 3.0 \text{ atom } \%$, a content of niobium (Nb) in a range represented by $1.0 \text{ atom } \% \leq Nb \leq 10.0 \text{ atom } \%$, a content of boron (B) in a range represented by $0.03 \text{ atom } \% \leq B \leq 2.2 \text{ atom } \%$, and the balance of titanium and unavoidable impurities;


melting said blank to provide a molten metal;

casting said molten metal to provide an ingot;

and

subjecting said ingot to a homogenizing thermal treatment.

TiAl-based intermetallic compound EP-592189

<ul style="list-style-type: none"> • Patent Assignee HONDA MOTOR • Inventor FUJIWARA YOSHIYA TOKUNE TOSHIO • International Patent Classification C22C-014/00 C22F-001/00 C22F-001/18 • US Patent Classification PCLO=148669000 PCLX=148421000 PCLX=420421000 • CPC Code C22F-001/18/3 	<ul style="list-style-type: none"> • Publication Information EP0592189 A1 1994-04-13 [EP-592189] <div style="text-align: right; margin-top: 5px;">  </div> <ul style="list-style-type: none"> • Priority Details 1992JP-0290800 1992-10-05 																								
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DE69319530	T2	1998-10-29	[DE69319530]																						

- **Abstract:**

(EP-592189)

A TiAl-based intermetallic compound has a metallographic structure which includes a region A having fine beta -phases dispersed in a gamma -phase. The volume fraction V_f of the beta -phases in the region A is set equal to or more than 0.1% ($V_f \geq 0.1\%$). Thus, the beta -phases can exhibit a pinning effect to prevent a transgranular pseudo cleavage fracture in the gamma -phase, thereby providing an enhanced high-temperature strength of the TiAl-based intermetallic compound.

Claims

(EP-592189)

1. A TiAl-based intermetallic compound with an excellent high-temperature strength, wherein said compound has a metallographic structure which comprises a region having fine beta -phases dispersed in a gamma -phase, the volume fraction V_f of beta -phases in said region being equal to or more than 0.1% ($V_f \geq 0.1\%$)
2. A TiAl-based intermetallic compound with an excellent high-temperature strength according to claim 1, wherein alpha 2 -phases are dispersed in the gamma -phase in said region.
3. A TiAl-based intermetallic compound with an excellent high-temperature strength, wherein said compound has a metallographic structure which comprises a first region having fine beta -phases dispersed in a gamma -phase, and a second region having a gamma -phase which does not include beta -phase, the volume fraction V_f of the beta -phases in said first region being equal to or more than 0.1% ($V_f \geq 0.1\%$).
4. A TiAl-based intermetallic compound with an excellent high-temperature strength according to claim 3, wherein alpha 2 -phases are dispersed in the gamma -phase in said first region.
5. A TiAl-based intermetallic compound with an excellent high-temperature strength according to claim 3 or 4, wherein the volume fraction V_f of said first region in said metallographic structure is equal to or more than 1% ($V_f \geq 1\%$).
6. A TiAl-based intermetallic compound with an excellent high-temperature strength according to claim 1, 2, 3 or 4, further including at least one beta -area enlarging element E selected from the group consisting of Mo, Nb, Ta, V, Co, Cr, Cu, Fe, Mn, Ni, Pb, Si and W, the content of said beta -area enlarging element E being equal to or more than 0.5 atomic % ($E \geq 0.5$ atomic %).
7. A process for producing a TiAl-based intermetallic compound with an excellent high-temperature strength, having a metallographic structure which comprises;
a first region consisting of either a region having fine beta -phases dispersed in a gamma -phase or a region having alpha 2 -phases and fine beta -phases dispersed in a gamma -phase, and a second region having a gamma -phase which does not include beta -phase, the volume fraction V_f of beta -phases in said first region being equal to or more than 0.1% ($V_f \geq 0.1\%$);

said process comprising:

a first step of subjecting a TiAl-based intermetallic compound blank having a metallographic structure including a gamma -phase and at least one of alpha 2 - and beta -phases to a solution treatment at a treatment temperature set in a range which permits alpha - and gamma -phases to be present;

quenching said TiAl-based intermetallic compound blank thereby providing an intermediate product having a metallographic structure including gamma -phases and supersaturated alpha 2 -phases;

and

a second step of subjecting said intermediate product to an artificial aging treatment at a temperature set in a range which permits alpha 2 - and gamma -phases to be present.

8. A process for producing a TiAl-based intermetallic compound with an excellent high-temperature strength according to claim 7, wherein the treatment temperature in said solution treatment is equal to or more than an eutectoid line EL which permits a reaction, alpha -phase + gamma -phase \rightarrow alpha 2 -phase + gamma -phase, to occur, but is equal to or less than alpha -trassus line TL which permits a reaction, alpha -phase \rightarrow alpha -phase + gamma -phase, to occur;
and the treatment temperature in said artificial aging treatment is equal to or more than 700 DEG.C, but is equal to or less than said eutectoid line EL .
9. A process for producing a TiAl-based intermetallic compound with an excellent high-temperature strength according to claim 7 or 8, wherein a cooling rate of said quenching is set higher than the cooling rate of an oil quenching.
10. A process for producing a TiAl-based intermetallic compound with an excellent high-temperature strength according to claim 7 or 8, wherein the heating time of said solution treatment is set equal to or more than 5 minutes.
11. A process for producing a TiAl-based intermetallic compound with an excellent high-temperature strength according to claim 7 or 8, wherein the heating time in said artificial aging treatment is set equal to or more than 5 minutes.
12. A process for producing a TiAl-based intermetallic compound with an excellent high-temperature strength according to claim 7 or 8, wherein said TiAl-based intermetallic compound blank further includes at least one beta -area enlarging element E selected from the group consisting of Mo, Nb, Ta, V, Co, Cr, Cu, Fe, Mn, Ni, Pb, Si and W, the content of said beta -area enlarging element E being equal to or more than 0.5 atomic % ($E \geq 0.5$ atomic %).

Claims

(JP2010270347)

1. Constitution Al: The TiAl alloy which consists of 8.0-9.5wt% and remainder Ti, in the 600-900.deg.C aging of 40 hours or more production method of the TiAl alloy for the inhalation and exhalation of air valve which features that it heat-treats.
2. When in the aforementioned constitution, furthermore, Fe, Cr and Mo, V, among Nb 1 kinds are added at least, the value of wt% of those addition quantities being used [for several 1] formulas below, in the claim 1 which features that the Mo equivalence becomes 5.7 or less production method of TiAl alloying for the inhalation and exhalation of air valve statement.

[Several 1]

$$\text{Mo equivalence} = \text{Mo} + 2.5\text{Fe} + 1.25\text{Cr} + 0.67\text{V} + 0.28\text{Nb}$$

3. Constitution Al: The TiAl alloy for the inhalation and exhalation of air valve which features that Ti₃Al of 30-50vol% is precipitating in .alpha.-Ti at the time of TiAl alloying which consists of 8.0-9.5wt% and remainder Ti.
4. In the aforementioned constitution, furthermore, Fe, Cr and Mo, V, being the TiAl alloy which among Nb at least adds 1 kinds, when using the value of wt% of those addition quantities [for several 2] formulas below, in the claim 3 which features that the Mo equivalence becomes 5.7 or less the TiAl alloy for the inhalation and exhalation of air valve of statement.

[Several 2]





$$\text{Mo equivalence} = \text{Mo} + 2.5\text{Fe} + 1.25\text{Cr} + 0.67\text{V} + 0.28\text{Nb}$$

Claims

(JP2010280927)

1. Al 40-42atom% and Cr: 2.4-2.6atom% it contains, the TiAl alloy where the remainder consists of Ti and the inevitable impurity, extrusion ratio 10 or more with the 1100-1150.deg.C, extrusion process and the description above which obtain the extrusion molding body the aforementioned compact being true aerial after the extrusion process ending, or in extrusion process the aforementioned compact where annealing process and the aforementioned annealing process which 2-5 time you keep with the 950-1050.deg.C end in the inert gas passing with the cooling process which cools at cooling rate of 10-60.deg.C/amount to the 400.deg.C, the TiAl alloy make internal combustion engine part which features that it is produced.
2. As for the aforementioned TiAl alloy, Nb: 1.3-1.9atom% and Zr: In the claim 1 which features that at least 1 kinds of 0.1-0.2atom% furthermore are contained the TiAl alloy make internal combustion engine part of statement.
3. In the claim 1 which features that aforementioned compact which passes the aforementioned cooling process the 20-35 volume % contains .beta.-Ti phase, at the same time .alpha.2 (Ti3Al) the 10-20 volume % contains phase or 2 the TiAl alloy make internal combustion engine part of statement.
4. The aforementioned internal combustion engine part, in either of the claim 1-3 which features that it is the valve or the piston pin the TiAl alloy make internal combustion engine part of statement.

Melting method of addition metal to TiAl based intermetallic JP08246081

<ul style="list-style-type: none"> • Patent Assignee HONDA MOTOR • Inventor IENAGA YUICHI NAKAGAWA TATSUYA FUJIWARA YOSHINARI TOKUNE TOSHIO SHIKAYA IZURU • International Patent Classification C22C-001/02 	<ul style="list-style-type: none"> • Publication Information JPH08246081 A 1996-09-24 [JP08246081]     • Priority Details 1995JP-0044370 1995-03-03 								
<ul style="list-style-type: none"> • Fampat family <table style="width: 100%; border: none;"> <tr> <td style="width: 30%;">JPH08246081</td> <td style="width: 10%; text-align: center;">A</td> <td style="width: 20%;">1996-09-24</td> <td style="width: 30%;">[JP08246081]</td> </tr> <tr> <td>JP3802579</td> <td style="text-align: center;">B2</td> <td>2006-07-26</td> <td>[JP3802579]</td> </tr> </table> 		JPH08246081	A	1996-09-24	[JP08246081]	JP3802579	B2	2006-07-26	[JP3802579]
JPH08246081	A	1996-09-24	[JP08246081]						
JP3802579	B2	2006-07-26	[JP3802579]						

- **Abstract:**

(JP08246081)

PURPOSE: To stably improve the yield of an additional metal, at the time of melting the additional metal having the m.p. higher than that of a metal as the essential component in the metal as the essential component, by pouring the green compact of the low m.p. easily meltable metal and the additional metal having higher m.p. into the molten metal of the additional metal having higher m.p. CONSTITUTION: For example, at the time of adding a Ti-Al intermetallic compound added with B having the m.p. higher than that of the same and executing melting in a molten metal M of the Ti-Al intermetallic compound, a small cylindrical green compact G composed the B powder and Al powder having the m.p. lower than the Ti-Al intermetallic compound is produced. When this green compact G is poured into the molten metal M of the Ti-Al intermetallic compound, the Al powder is melted, and simultaneously, the B powder in the vicinity of the same is also divided individually, which is brought into contact with the molten metal M, and melted. Thus, the B powder can be melted without generating the remainder of its melting in a relatively short period.

Claims

(JP08246081)

1. In basis metal, that basis metal compared to high

When it is and it melts the addition metal which possesses fusion point, the aforementioned addition gold

The divination which possesses the fusion point which is lower than the being attached powder and the aforementioned basis metal

The compact which consists of with the powder of the molten characteristic metal, the aforementioned basis metal

The addition metal which features that it throws in the hot water melting

Law.

2. The aforementioned basis metal Ti or TiAl system

It is one kind of intermetallic, the aforementioned addition metal is B,

The aforementioned fusible characteristic metal is Al, the addition metal of claim 1 statement

Melting method.

3. Manufacturing the hot water of the aforementioned basis metal and the description above

In melting of the addition metal, [indakushiyo] which has the water cooling crucible

It can use the [nsukaru] fusion furnace, claim 1 or 2 statements

Melting method of addition metal.

Claims

(JP08238538)

1. Ti or Ti alloy or TiAl system

The core which is used for casting the hollow molding which consists of the intermetallic

So being, to be constituted from the Fe based alloy material, at the same time the aforementioned air

The molding (1) the cubic measure ratio R for cubic measure is $R \geq 17\%$

Thing is featured, Ti or Ti alloy or TiAl

Core for Fe based intermetallic hollow molding casting.

2. As for the aforementioned Fe based alloy material, rolling the general structure

Steel and general steel for cold finished steel bars, cold finished steel bars, [kuromumori]

The kind which is selected from the [buden] steel steel or the stainless steel stick

So it is, Ti or Ti alloy or T of claim 1 statement

Core for TiAl based intermetallic hollow molding casting.

3. Mold for centrifugal casting (M) with component [a]

[ru], claim Ti or Ti alloy of 1 or 2 statements and

Core for TiAl based intermetallic hollow molding casting.

Claims

(JP07233431)

1. I [2] the body of the lamella phase which consists of phase and I phase

The matrix where integral calculus ratio V_f is $V_f \geq 15\%$ and, that

To disperse to the matrix, at the same time cubic measure amount ratio V_f the $0.1\% \leq$

It features that it possesses TiB which is $V_f \leq 15\%$

High intensity, high ductile TiAl based intermetallic.

2. The cubic measure amount ratio V of TiB in all boride

f is $V_f \geq 30\%$, high intensity of claim 1 statement, high extending

Characteristic TiAl based intermetallic.

Claims

(JP06228705)

1. Al content 38 atmoic % $\leq Al \leq 52$ field

The child % being, metallographic structure the layer where I [2] phase and I phase form layer

To possess the condition organizational limits, the nitride to disperse to those stratified organizational limits, the [so]

Cubic measure amount ratio V of nitride [2] with $0.01\% \leq V [2] \leq 15\%$

Conversion between the high intensity high ductile TiAl metal which feature a certain thing

Combination ones.

2. Cubic measure amount ratio V of the aforementioned stratified organizational limits [1] V [1] a prg.

It is 5%, the high intensity high ductile TiAl gold of claim 1 statement

Intergeneric chemical compound.

3. The aforementioned nitride is placed next phase of the aforementioned stratified organizational limits

In order to parallel to the boundary of 2 phases, to include the needle-shaped nitride which extends, that

In the nitride ratio R of the aforementioned needle-shaped nitride [1], the aforementioned nitrating

When designating the cubic measure amount ratio of the thing as V [2], with R [1] $\leq 0.6V [2]$ the [a]

[ru], claim high intensity high ductile TiAl gold of 1 or 2 statements

Intergeneric chemical compound.

4. The aforementioned nitride to include Ti [3] AlN, that

In the nitride the ratio R of Ti [3] AlN [2], the aforementioned nitride

When designating cubic measure amount ratio as V [2], with R [2] $\leq 0.6V [2]$ the [a]

[ru], claim high intensity high ductility TiAl of 1,2 or 3 statements

Type intermetallic.

5. Al content 38 atmoic % $\leq Al \leq 52$ field

The child % being, metallographic structure the layer where I [2] phase and I phase form layer

To possess the condition organizational limits, in those stratified organizational limits the nitride and boride

The thing to disperse, cubic measure amount ratio the body of V of that nitride [2] and boride

Harmony V of integral calculus ratio V [5] [2] $+V [5] 0.01\% \leq V [2] +V [5]$

The high intensity high ductility TiAl which features that it is the $\leq 15\%$

Type intermetallic.

6. The lower limit value of Al content 46 atmoic % $\leq Al$

The ≤ 48 atmoic % there to be a range, in addition upper limit of Al content

49 atmoic % $\leq Al \leq 52$ atmoic % there being a range, metal group

Weaving to possess the stratified organizational limits where I [2] phase and I phase form layer, that

In the material which the nitride disperses to the stratified organizational limits, the primary thermal place

Reason, to administer the secondary heat treatment which it comes after that, heat treatment of primary heat treatment

Temperature T [1], it is parent phase of I [2] phase, cubic measure amount ratio V of I phase [3]

With ratio V [3] /V with the cubic measure amount ratio V of I phase [4] [4] $0.5 \leq V [3]$

Setting to the temperature limits which are the /V [4] ≤ 2 , the body of the aforementioned stratified organizational limits

To adjust integral calculus ratio V [1], heat treatment temperature T of secondary heat treatment [2]

Compared to heat treatment temperature [1] above the 50.deg.C it is lower T of primary heat treatment

Setting to the temperature limits, cubic measure amount ratio V of the aforementioned nitride [2] and precipitation

The high intensity high ductility TiA which features that you adjust form

Production method of I based intermetallic.

7. The lower limit value of Al content 42 atmoic % $\leq Al$

The ≤ 45 atmoic % there to be a range, in addition upper limit of Al content

46 atmoic % $\leq Al \leq 48$ atmoic % there being a range, metal group

Weaving to possess the stratified organizational limits where I [2] phase and I phase form layer, that

In the material which the nitride disperses to the stratified organizational limits, the primary thermal place

Reason, to administer the secondary heat treatment which it comes after that, heat treatment of primary heat treatment

Temperature T [1], it is parent phase of I [2] phase, cubic measure amount ratio V of I phase [3]

With ratio V [3] /V with the cubic measure amount ratio V of I phase [4] [4] $V [3] /V [4] =$

2 setting to the temperature limits below the temperature which is and above the 900.deg.C, before

To adjust the cubic measure amount ratio V of the description stratified organizational limits [1], secondary heat treatment

Heat treatment temperature T [2], from heat treatment temperature T of primary heat treatment [1]

Above the 50.deg.C setting to the low temperature limits, cubic measure amount of the aforementioned nitride

Ratio it features that adjusts V [2] and precipitation form, high

Production method of strength high ductile TiAl based intermetallic.

8. The lower limit value of Al content 38 atmoic % $\leq Al$

The ≤ 42.5 atmoic % there to be a range, in addition the upper limit of Al content

Value 42.5 atmoic % $\leq Al \leq 45$ atmoic % in range oh

The [te], metallographic structure the stratified organizational limits where I [2] phase and I phase form layer

In the material which the nitride disperses to the possessing and the stratified organizational limits,

To administer primary heat treatment and the secondary heat treatment which it comes after that, primary heat treatment

Heat treatment temperature T [1], (.alpha.+gamma.) from phase (I [2] +.gamma.) phase

When to phase changing, rule - below irregular transformation point Tr, 90

Setting to the temperature limits above the 0.deg.C, cubic measure amount ratio of the aforementioned stratified organizational limits

[1] to adjust V, heat treatment temperature T of secondary heat treatment [2], 1

The temperature limits which compared to heat treatment temperature [1] above the 50.deg.C are lower T of the next heat treatment

Setting, cubic measure amount ratio V of the aforementioned nitride [2] and precipitation form

The high intensity high ductile TiAl gold which features that you adjust

Production method of intergeneric chemical compound.

9. As the aforementioned material, nitriding to the aforementioned stratified organizational limits

Those which the thing and boride are dispersed are used, the claim

Conversion between high intensity high ductile TiAl metal of 6,7 or 8 statements

Production method of combination ones.

Claims

(JP06228685)

1. Al and Cr and Nb, Ta and W and

Is selected from Mo at least to contain with the kind which, the remainder
Being Ti and the inevitable impurity,Al content 42 atmoic % \leq Al \leq 46 atmoic %,Cr content 1 atmoic % \leq Cr \leq 4 atmoic %,Nb content 1 atmoic % \leq Nb \leq 4 atmoic %,Ta content 0.3 atmoic % \leq Ta \leq 4 atmoic %,W content 0.05 atmoic % \leq W \leq 4 atmoic %,Mo content 0.5 atmoic % \leq Mo \leq 4 atmoic %between the high intensity high ductile TiAl metal which feature that is
Chemical compound.

2. Metallographic structure, I phase and I [2] phase and I phase

At least it consists of with one side, high intensity of claim 1 statement high
Ductile TiAl based intermetallic.

3. Al and Cr and Nb, Ta and W and

Is selected from Mo at least to contain with the kind which, the remainder
Being Ti and the inevitable impurity,Al content 42 atmoic % \leq Al \leq 46 atmoic %,Cr content 1 atmoic % \leq Cr \leq 4 atmoic %,Nb content 1 atmoic % \leq Nb \leq 4 atmoic %,Ta content 0.3 atmoic % \leq Ta \leq 4 atmoic %,W content 0.05 atmoic % \leq W \leq 4 atmoic %,Mo content 0.5 atmoic % \leq Mo \leq 4 atmoic %

in the material which is primary heat treatment and the secondary heat treatment which it comes after that

To do, heat treatment temperature T of primary heat treatment [1], at parent phase of I [2] phase

Cubic measure amount ratio I of a certain I phase ratio α/γ . with the cubic measure amount ratio I of I phaseTo set to the temperature limits which are $0.5 \leq \alpha/\gamma \leq 3$, the secondary thermal place

Heat treatment temperature T of reason [2], I [2] phase to exist, at the same time the primary thermal place

It sets to the temperature limits which compared to heat treatment temperature [1] above the 50.deg.C are lower T of reason

Conversion between the high intensity high ductile TiAl metal which feature that it does

Production method of combination ones.

4. Al and Cr and Nb, Ta and W and

Is selected from Mo at least to contain with the kind which, the remainder
Being Ti and the inevitable impurity,Al content 42 atmoic % \leq Al \leq 46 atmoic %,Cr content 1 atmoic % \leq Cr \leq 4 atmoic %,Nb content 1 atmoic % \leq Nb \leq 4 atmoic %,Ta content 0.3 atmoic % \leq Ta \leq 4 atmoic %,W content 0.05 atmoic % \leq W \leq 4 atmoic %,Mo content 0.5 atmoic % \leq Mo \leq 4 atmoic %

in the material which is primary heat treatment and the secondary heat treatment which it comes after that

To do, heat treatment temperature T of primary heat treatment [1], cubic measure amount ratio of I [2] phase

I [2] ratio I with the cubic measure amount ratio I of I phase [2]/ γ . $0.5 \leq \alpha$. [2]To set to the temperature limits which are $\alpha/\gamma \leq 3$, heat treatment of secondary heat treatment warm

Degree T [2] heat treatment temperature T of primary heat treatment [1] compared to above 50.deg.C

The high intensity high ductility T which features that it sets to the low temperature limits

Production method of iAl based intermetallic.

Claims

(JP06049570)

Claims machine translated from Japanese

1. Metallographic structure plural 1st stratified organizational territories (R [1]) With the plural 2nd stratified organizational territories (R [2]) with to possess, each 1 stratified organizational territories (R [1]) TiAl phase (La) with Ti [3] Al phase (Lb) with, those lamination directions (A) is unidirectional That in order to become, laminating alternately, to be constituted, each 2nd stratified organization Territory (R [2]) TiAl phase (La) with Ti [3] Al phase (L b) That laminating alternately, the plural stratified organizational sections which become (L) The [ri] to be constituted, those stratified organizational sections (L), the description above 2nd stratified The organizational territory (R [2]) in the aforementioned both phases (La and Lb) the product In order layer direction (A) to become irregular, it is arranged The high intensity high *** characteristic TiAl based intermetallic which is featured.
2. The aforementioned 2nd stratified organizational territory (R [2]) cubic measure amount Ratio Vf is $0.1\% \leq Vf < 100\%$, claim 1 description High intensity high *** characteristic TiAl based intermetallic of *** .
3. The aforementioned 2nd stratified organizational territory (R [2]) cubic measure amount Ratio Vf is $20\% \leq Vf$, high intensity of claim 2 statement high *** characteristic TiAl based intermetallic.
4. Metallographic structure TiAl phase (La) with Ti [3] Al phase (Lb) with laminating alternately, the plural stratified organizations which become The section (L) from to be constituted, those stratified organizational sections (L) the description above Both phases (La and Lb) lamination direction (A) becomes irregular The sea urchin to be arranged, the aforementioned stratified organizational section (L) grain size D $D \leq 5$ The high intensity high *** characteristic which features that it is set to 0 .micro.m TiAl based intermetallic.

Claims

(JP06049567)

Claims machine translated from Japanese

1. Metallographic structure plural stratified organizational territories (R [L])

To possess, as for each stratified organizational territory (R [L]) TiAl phase (La)

With laminating with Ti [3] Al phase (Lb) alternately, the plural which becomes

From the stratified organizational section (L) to be constituted, those stratified organizational sections

(L) In the aforementioned stratified organizational territory (R [L]) the aforementioned both phases

Way (the lamination direction of La and Lb) (A) becomes irregular,

The high intensity TiAl metal which features that it is arranged

Between chemical compound.

2. Cubic measure amount ratio V of the aforementioned stratified organizational territory (R [L])

f is $V_f \geq 0.5\%$, high intensity Ti of claim 1 statement

Al based intermetallic.

Claims

(JP06049566)

Claims machine translated from Japanese

1. Metallographic structure plural 1st organizational territories (R [1])

That to possess with the plural 2nd organizational territories (R [2]), each 1st organizational territory

As for limits (R [1]) axial crystal and plural Ti such as plural TiAl [3]

Axial crystal such as Al to be constituted at least from one side, each 2nd organization

As for territory (R [2]) TiAl phase (La) and Ti [3] Al phase (L

b) That laminating alternately, the plural stratified organizational sections (L) which become

The [ri] to be constituted, as for those stratified organizational sections (L), the aforementioned 2nd organization

In the territory (R [2]) the aforementioned both phases (La and Lb) lamination

In order direction (A) to become irregular, being arranged special

The high ductile TiAl based intermetallic which is made collection/symbol.

2. Cubic measure amount ratio V of the aforementioned 2nd organizational territory (R [2])

f is $0.1\% \leq Vf \leq 95\%$, claim 1 statement high

Ductile TiAl based intermetallic.

Claims

(JP05065581)

Claims machine translated from Japanese

1. Surface layer axial crystal under mean diameter 50 .micro.m and the like

From to constitute, as for that and the like axial crystal I and so on the axial crystal and I [2] and so on the axial crystal

Conversion between the high fatigue strength TiAl metal which feature that it becomes the [ri]

Combination ones.

2. The description above I [2] and so on cubic measure amount ratio Vf of axial crystal $2\% \leq$

It set to $V_f \leq 20\%$, high fatigue strength T of claim 1 statement

iAl based intermetallic.

Claims

(JP05065580)

1. Metallographic structure, I [2] phase and I phase alternately

The TiAl metal which consists of with stratified organization and I and so on the axial crystal which it laminates

In between chemical compound, I and so on cubic measure amount ratio Vf of the axial crystal $3\% \leq V$

To set to $f \leq 90\%$, at least in portion of the aforementioned metallographic structure

It features that the aggregate of the aforementioned stratified organization is made to disperse high

Strength high ductile TiAl based intermetallic.

Claims

(JP05065573)

1. Stratified I [2] phase and I phase are laminated alternately

Organization and, I [2] and so on the axial crystal and I and so on the mixed crystal organization which consists of the axial crystal

It is while the possessing and the aforementioned stratified organization, cubic measure amount ratio of I [2] phase V_{f1}

It does, in addition it is in the midst of the aforementioned mixed crystal organizing, I [2] and so on cubic measure amount ratio of the axial crystal V_f

When making 2,

$0.05\% \leq V_{f1} + V_{f2} < 50\%$, and $0.6V$

The high

characteristic TiAl system which features that it is formed the relationship of $f_2 \leq V_{f1}$

Intermetallic.

Claims

(JP05065562)

Claims machine translated from Japanese

1. Chemical combination between the metal where crystalline structure is I single-phase structure

Thing make 1Ti-Al powder and crystalline structure with I [2] single-phase structure

The raw materials which possess with a certain intermetallic make 2Ti-Al powder

To produce the material making use of the powder, next in the aforementioned material calcination processing

Administering, and so on it consists of the axial crystal, at the same time does not have the direction dependency

It features that the structural element which has metallographic structure is obtained high it is strong

Production method of degree TiAl based intermetallic make structural element.

2. The 2Ti-Al powder in the raw materials powder

40 weight % of combination quantity is set below, claim 1 statement high

Production method of strength TiAl based intermetallic make structural element.

3. Crystalline structure I phase and I [2] phase random

To be quarter-phase structure which arranges, at the same time cubic measure amount ratio Vf of I [2] phase

The intermetallic make 1Ti-A which is set 30% or less

The intermetallic where the I powder and crystalline structure are I [2] single-phase structure

Make making use of the raw materials powder which possesses with the 2Ti-Al powder the material

To produce, administering calcination processing to the aforementioned material next, and so on, the axial crystal

It consisted of, it had the metallographic structure which at the same time does not have the direction dependency

The high intensity TiAl metal which features that the structural element is obtained

Production method of between chemical compound make structural element.

4. In the raw materials powder, the gross of I [2] phase 40

Weight % It sets below, high intensity TiAl of claim 3 statement

Production method of type intermetallic make structural element.

Claims

(JP05065559)

1. Ti powder and Al powder and Ti and A

At least one side of the l powder and the powder of the element which causes the eutectoid reaction

To form the material with making use of the raw materials powder which consists of, next the description above

High intensity TiAl it features that calcination treatment is administered to the material

Production method of type intermetallic.

2. As for the powder of the element which causes the aforementioned eutectoid reaction, M


It is selected from the n powder, the Si powder and the Ge powder little

Also to be kind, the addition quantity of that powder 0.05 atmoic % from here

On, 5 atmoic % it is set below, high intensity of claim 1 statement

Production method of TiAl based intermetallic.

High strength tial alloy JP05065579

<ul style="list-style-type: none"> • Patent Assignee HONDA MOTOR • Inventor TOKUNE TOSHIO TSUNASHIMA SAKAE FUJIWARA YOSHINARI • International Patent Classification C22C-001/00 C22C-001/10 C22C-014/00 C22C-029/02 C22C-029/06 C22C-029/18 C22C-032/00 	<ul style="list-style-type: none"> • Publication Information JPH0565579 A 1993-03-19 [JP05065579]  <ul style="list-style-type: none"> • Priority Details 1991JP-0256969 1991-09-09
<ul style="list-style-type: none"> • Fampat family JPH0565579 A 1993-03-19 [JP05065579] 	

- **Abstract:**
(JP05065579)
PURPOSE: To obtain a high strength TiAl alloy by incorporating a specified amt. of particles of a compd. contg. Ge, C or Si.
CONSTITUTION: This TiAl alloy contains 0.01-15vol.% particles of a compd. contg. at least one or more among Ge, C and Si and has high strength. The particles are dispersed as deposited phase in this TiAl alloy. In the case of <0.01vol.% of the particles, high strength is not obtd. In the case of >15vol.%, strength is reduced on the contrary. COPYRIGHT: (C)1993,JPO&Japio

Claims

(JP05065579)

1. Ge, C, among Si at least above kind

The chemical compound grain which includes the element vis-a-vis the whole alloy the 0.01-1
5 volume % the high intensity TiAl combination which features that it contains
Gold.

Claims

(JP05065578)

1. The TiAl based alloy of possessing lamella organization

It is in the [te] and the aforementioned lamella organization, width of I phase something related to width of I [2] phase

Value (of width of width/.gamma. phase of I [2] phase) 0.01 or more,

0.55 It is below, at the same time is while the aforementioned lamella organizing I [2] phase

Cubic measure ratio 0.05% from here vis-a-vis the cubic measure of the aforementioned lamella organization

The high characteristic TiAl which features that on and it is 32% or less

Type alloy.

2. In high characteristic TiAl based alloy of claim 1 statement

Being, cubic measure ratio of lamella organization vis-a-vis alloy the whole description above 30

% The high characteristic TiAl based alloy which features that it is above.

Claims

(JP05065577)

Claims machine translated from Japanese

1. The TiAl based alloy smelt of possessing lamella organization

Width of one I phase which it adjoins in inside the [te] and the aforementioned lamella organization

With total of width of one I [2] phase 0.01 .micro.m or more, 30.micro.

It is m, or less at the same time is while the aforementioned lamella organizing cubic measure ratio of I [2] phase

Vis-a-vis the cubic measure of the aforementioned lamella organization 0.05% or more, 40


% The high ductile TiAl based alloy which features that it is below.

2. In high ductile TiAl based alloy of claim 1 statement

Being, cubic measure ratio of lamella organization vis-a-vis alloy the whole description above 30

% The high ductile TiAl based alloy which features that it is above.

High strength tial intermetallic compound JP05065571

<ul style="list-style-type: none"> • Patent Assignee HONDA MOTOR • Inventor FUJIWARA YOSHINARI TSUNASHIMA SAKAE TOKUNE TOSHIO • International Patent Classification C22C-014/00 C22F-001/00 C22F-001/18 	<ul style="list-style-type: none"> • Publication Information JPH0565571 A 1993-03-19 [JP05065571] <div style="text-align: right; margin-top: 5px;">  </div> <ul style="list-style-type: none"> • Priority Details 1991JP-0227728 1991-09-09
<ul style="list-style-type: none"> • Fampat family JPH0565571 A 1993-03-19 [JP05065571] 	

- **Abstract:**
(JP05065571)
PURPOSE: To provide a high strength TiAl intermetallic compd.
CONSTITUTION: The compsn. of a base part 1 is composed of 46-50 atomic % Al and the balance Ti. The compsn. of a surface layer part 2 integrated with the base part 1 is composed of 42-48 atomic % Al and the balance Ti and the Ti content of the surface layer part 2 is made higher than that of the base part 1. Since the base part 1 has a higher Al content than the surface layer part 2, satisfactory ductility is exhibited. Since the surface layer part 2 has a higher Ti content than the base part 1, satisfactory strength at ordinary temp. is exhibited. Thus, the objective TiAl intermetallic compd. having enhanced strength as a whole can be provided. COPYRIGHT: (C)1993,JPO&Japio

Claims

(JP05065571)

Claims machine translated from Japanese

1. Constitution of active section 46 atmoic % $\leq Al \leq 50$

Atmoic % And to be remainder Ti, the aforementioned active section and the surface of one body

Constitution of section 42 atmoic % $\leq Al \leq 48$ atmoic % and remainder T

To be i, at the same time Ti content Ti content of the aforementioned active section

In order also for the [ri] to become many, it features that it is set high

Strength TiAl based intermetallic.

Claims

(JP05065570)

Claims machine translated from Japanese

1. At least part Ti [3] Al phase and TiAl

To be constituted from the stratified organization which laminates with I phase alternately, the layer of that

At the time of condition organizing, Ti [3] Al phase and TiAl phase lamination

Width of the direction which designates the width of direction as a, in addition the lamination direction crosses

When making b, aspect ratio a/b $0.2 \leq a/b$ The high *** ductility TiAl which features that it sets to the ≤ 1.3

Type intermetallic.

2. Cubic measure amount ratio V_f of the aforementioned stratified organization, 10%It is $\leq V_f \leq 100\%$, high *** ductility Ti of claim 1 statement

Al based intermetallic.

3. Ti in the aforementioned stratified organizing [3] the body of Al phase

Integral calculus ratio V_f , is $0.5\% \leq V_f \leq 50\%$, the claim

High *** ductile TiAl based intermetallic of 1 or 2 statements.

Claims

(JP05065569)

Claims machine translated from Japanese

1. Ti [3] Al phase (p1) and TiAl phase (p

2) With to possess the stratified organization (L) which is laminated alternately, the layer of that
Cubic measure amount ratio V_f of Ti [3] Al phase (p1) in the midst of condition organization (L)
Ti which it sets to $0.05\% \leq V_f \leq 40\%$, in addition phase is placed next

[3] Al phase (p1) and TiAl phase (p2) lamination [yunitsu]

When making [to] (U), Ti [3] Al phase (p1) and TiAl

The aforementioned lamination unit in the lamination direction of phase (p2)

(U) Setting average width w to $0.01 \text{ .micro.m} \leq w \leq 30 \text{ .micro.m}$

The high *** characteristic TiAl based intermetallic which features that it does.

2. Cubic measure amount ratio V_f of the aforementioned stratified organization (L) 3It set to $0\% \leq V_f \leq 100\%$, claim 1 statement high ***

Characteristic TiAl based intermetallic.

Claims

(JP05065560)

Claims machine translated from Japanese

1. Constitution 42 atmoic % \leq Al \leq 47 atmoic %

Are calling remainder Ti the 1st powder and the constitution which 46 atmoic % \leq A

To be \leq 49 atmoic % and remainder Ti, at the same time Ti content

It was set fewer than Ti contents of the aforementioned 1st powder

As it possesses with 2 powders, the combination quantity of aforementioned 1st powder 20 it is heavy

The quantitative % \leq 1st powder \leq 70 weight % from the raw materials powder which is set

The material forming, next administering calcination processing to that material

Production of the high intensity high ductile TiAl based intermetallic which is made feature

Method.

Claims

(JP05065561)

Claims machine translated from Japanese

1. Ti [3] Al phase and TiAl phase alternately product

To possess the stratified organization which layer is done, at the same time 0.1 atomic % of Ge content

$\leq \text{Ge} \leq 0.5$ atomic % it produces the material which is set, the next is

So administering heat treatment to the aforementioned material, mean diameter of the aforementioned stratified organization

While controlling increase, the product of Ti [3] Al phase and TiAl phase

Average width of the TiAl phase in layer direction, the description above of the aforementioned material

The high creeping strength which features that average width compared to it expands

Production method of the TiAl based intermetallic which it possesses.

Claims

(JP05065576)

1. Metallographic structure, heat treatment TiAl phase I pro-eutectoid

TiAl phase I ' with from the TiAl based intermetallic which is formed

So being, the aforementioned pro-eutectoid TiAl phase I ' cubic measure amount ratio Vf 4

The high ductility TiAl which features that it sets 0% or less

Type intermetallic.

2. Metallographic structure, matrix phase M and the [ma]

The pro-eutectoid TiAl phase I which is dispersed to [toritsukusu] phase M ' with from structure

As for forming and the aforementioned matrix phase M heat treatment TiAl phase I

With the TiAl based intermetallic which possesses [bi] Ti [3] Al phase I [2]

Being, the pro-eutectoid TiAl phase I in metallographic structure the whole description above '





To set cubic measure amount ratio Vf 40% or less, in addition aforementioned [matori]

Cubic measure amount ratio Vf of the Ti [3] Al phase I in [tsukusu] phase M [2]

The high ductility TiA which features that it sets 50% or less

I based intermetallic.

Structural member made of tial intermetallic compound JP05065575

<ul style="list-style-type: none"> • Patent Assignee HONDA MOTOR • Inventor FUJIWARA YOSHINARI TOKUNE TOSHIO TSUNASHIMA SAKAE • International Patent Classification C22C-014/00 C22F-001/00 C22F-001/18 	<ul style="list-style-type: none"> • Publication Information JPH0565575 A 1993-03-19 [JP05065575]     • Priority Details 1991JP-0250281 1991-09-04
<ul style="list-style-type: none"> • Fampat family JPH0565575 A 1993-03-19 [JP05065575] 	

- **Abstract:**

(JP05065575)

PURPOSE: To provide a structural member made of a high strength and high toughness TiAl intermetallic compd.
 CONSTITUTION: This structural member 1 used under prescribed stress is made of a TiAl intermetallic compd. having a lamellar structure L formed by alternately laminating Ti(sub 3)Al phase .alpha.(sub 2) and TiAl phase .gamma.. The volume fraction Vf of the lamellar structure L is set 100% and the angle .theta. of inclination of a laminating direction line (b) to a line (a) of stress in the structure L is 90 deg. when the stress direction (a) is defined to be parallel to the stress direction in the lamellar structure L and when the laminating direction line (b) is defined to be parallel to the alternately laminating direction of the Ti(sub 3)Al phase .alpha.(sub 2) and the TiAl phase .gamma..
 COPYRIGHT: (C)1993,JPO&Japio

Claims

(JP05065575)

1. Ti [3] Al phase (I [2]) and TiAl phase

(I) Ti which possesses the stratified organization (L) which is laminated alternately

Is formed being the structural element which from the Al based intermetallic,

As for the aforementioned stratified organization (L) plural stratified histodifferentiation departments (La)

The [ri] is constituted, in all the stratified histodifferentiation departments (La) Ti [3] which

Al phase I [2] setting the lamination direction of TiAl phase I unidirectionally

The TiAl based intermetallic make structure division which features that it does

Material.

2. TiAl phase (I [2]) and TiAl phase (I)

With the TiAl system which possesses the stratified organization (L) which is laminated alternately

To be constituted from the intermetallic, at the same time under specified stress use

Being the [re] [ru] structural element, cubic measure amount ratio of the aforementioned stratified organization (L)

Vf to be $30\% \leq Vf \leq 100\%$, the aforementioned stratified organization

(L) Parallel with the stress direction in stress directional traverse (a) correcting/rule

Fixed to do, in addition Ti [3] Al phase (I [2]) and TiAl phase (I)

When stipulating the lamination directional traverse (b) parallel with lamination direction,

The aforementioned lamination directional traverse (b) for the aforementioned stress directional traverse (a)

It features that tilted angle θ is $45.\text{deg.} \leq \theta \leq 90.\text{deg.}$

TiAl based intermetallic make structural element.

3. As for the aforementioned TiAl based intermetallic, Ti

Combining, by forming the Ti [5] M [3] type deposit the description above

Ti [3] Al phase (I [2]) and TiAl in stratified organization (L)

The 3rd element which arranges the lamination direction of I phase (I) unidirectionally

(M) To contain, as for content of that 3rd element (M) 0.0

5 atmoic % $\leq M \leq 0.5$ atmoic % is, claim 1 or 2

TiAl based intermetallic make structural element of statement.





4. Ti [3] in the aforementioned stratified organization (L) Al

Of phase (I [2]) cubic measure amount ratio Vf is $Vf \leq 80\%$, claim

Section TiAl based intermetallic make structure of 1,2 or 3 statements

Component.

High toughness and high ductility tial intermetallic compound JP05065574

<ul style="list-style-type: none"> • Patent Assignee HONDA MOTOR • Inventor TSUNASHIMA SAKAE FUJIWARA YOSHINARI TOKUNE TOSHIO • International Patent Classification C22C-001/04 C22C-014/00 C22F-001/00 C22F-001/18 	<ul style="list-style-type: none"> • Publication Information JPH0565574 A 1993-03-19 [JP05065574]     • Priority Details 1991JP-0250280 1991-09-04
<ul style="list-style-type: none"> • Fampat family JPH0565574 A 1993-03-19 [JP05065574] 	

- **Abstract:**

(JP05065574)





PURPOSE: To provide a TiAl intermetallic compd. having excellent toughness and ductility. CONSTITUTION: The metal texture of this TiAl intermetallic compd. is composed of a group of parts L having a lamellar structure formed by alternately depositing platy TiAl phase .gamma. and platy Ti(sub 3)Al phase .alpha.(sub 2), TiAl phase .gamma.' forming a group of equiaxed crystals and existing among the parts L and amorphous Ti(sub 3)Al phase .alpha.(sub 2)' filling the gap among the equiaxed crystals. The parts L have satisfactory toughness and ductility owing to their own laminated structure. The brittleness of this TiAl intermetallic compd. due to the TiAl phase .gamma.' can be compensated by regulating the volume fraction Vf of the amorphous Ti(sub 3)Al phase .alpha.(sub 2)' to 0.5-50%. COPYRIGHT: (C)1993,JPO&Japio

Claims

(JP05065574)

1. Axial crystal TiAl phase I of one group and the like ' with, those
And so on axial crystal TiAl phase I ' the uncertain shape Ti [3] Al phase I which buries between
[2] ' With to possess, the uncertain shape Ti [3] Al phase I [2] ' cubic measure amount
Ratio Vf 0.5% or more and setting 50% or less special
The high ductile TiAl based intermetallic which is made collection/symbol.

Oxidation resistant tial intermetallic compound material and production of it JP05059464

<ul style="list-style-type: none"> • <u>Patent Assignee</u> HONDA MOTOR • <u>Inventor</u> FUJIWARA YOSHINARI TOKUNE TOSHIO TSUNASHIMA SAKAE • <u>International Patent Classification</u> C22C-001/00 	<ul style="list-style-type: none"> • <u>Publication Information</u> JPH0559464 A 1993-03-09 [JP05059464]     • <u>Priority Details</u> 1991JP-0242362 1991-08-29
<ul style="list-style-type: none"> • <u>Fampat family</u> JPH0559464 A 1993-03-09 [JP05059464] 	

- **Abstract:**

(JP05059464)

PURPOSE: To provide a TiAl intermetallic compd. material having excellent oxidation resistance at high temp.
 CONSTITUTION: A middle layer 2 of Al(sub 2)Ti as an intermetallic compd. is formed on a substrate 1 of TiAl as an intermetallic compd. so that the layer 2 is integrated with the substrate 1 and a surface layer 3 of (Al, Ge)(sub 3)Ti as an intermetallic compd. is formed on the middle layer 2 so that the layer 3 is integrated with the layer 2. The surface layer 3 is very dense and has function to prevent the penetration and diffusion of oxygen from the outside. The middle layer 2 has function to prevent the oxidation of the substrate 1. COPYRIGHT: (C)1993,JPO&Japio

Claims

(JP05059464)

1. The subject which consists of the TiAl based intermetallic

(1) With, (Al and Ge) [3] from Ti based intermetallic

The [ri], at the same time the aforementioned subject (1) with the surface of one body (3) with having
The oxidation resistance TiAl based intermetallic which features that it is
Material.

2. The subject which consists of the TiAl based intermetallic

(1) With, from the TiAl based intermetallic whose Al density is high

To become, at the same time the aforementioned subject (1) with center of one body (2) with,
(Al and Ge) [3] to consist of the Ti based intermetallic, at the same time before
Description center (2) with the surface of one body (3) with have
The oxidation resistance TiAl based intermetallic material which is featured.


3. 25 atmoic % above, 75 atmoic % Al below

It contains, the TiAl based intermetallic group where the remainder is Ti
Component and 0.01 atmoic % above, 1 atmoic % Ge below

To produce the intermediate material which it contains, next in the aforementioned intermediate material heat treatment
Administering, (Al and Ge) [3] it consists of the Ti based intermetallic
The oxidation resistance TiAl gold which features that the surface is formed
Production method of intergeneric chemical compound material.

High toughness and high ductility tial intermetallic compound

JP05059476

<ul style="list-style-type: none"> • Patent Assignee HONDA MOTOR • Inventor FUJIWARA YOSHINARI TOKUNE TOSHIO TSUNASHIMA SAKAE • International Patent Classification C22C-021/00 	<ul style="list-style-type: none"> • Publication Information JPH0559476 A 1993-03-09 [JP05059476]  <ul style="list-style-type: none"> • Priority Details 1991JP-0240251 1991-08-28 				
<ul style="list-style-type: none"> • Fampat family <table style="width: 100%; border: none;"> <tr> <td style="text-align: left;">JPH0559476</td> <td style="text-align: center;">A</td> <td style="text-align: center;">1993-03-09</td> <td style="text-align: right;">[JP05059476]</td> </tr> </table> 		JPH0559476	A	1993-03-09	[JP05059476]
JPH0559476	A	1993-03-09	[JP05059476]		

- **Abstract:**
(JP05059476)
PURPOSE: To provide a TiAl intermetallic compd. having excellent toughness and ductility. CONSTITUTION: This TiAl intermetallic compd. is made of Li(sub 2) phase A obtd. by incorporating Mn into Al(sub 3)Ti phase. The Li(sub 2) phase A has double-phase structure having matrix forming regions a(sub 1) and a network forming region a(sub 2) having a higher Mn concn. than the regions a(sub 1). COPYRIGHT: (C)1993,JPO&Japio

Claims

(JP05059476)

1. Al [3] in Ti phase, from Cr and Mn selection

L1 which at least makes a kind of 3rd element contain [2]

To be constituted from phase, the L1 [2] as for phase, density of the 3rd element uncommonness

The high ductility T which possessing the plural constitution limits which are done feature is done
iAl based intermetallic.

2. 60 atmoic % above, 67 atmoic % Al below

And 8 atmoic % above, 15 atmoic % containing the 3rd element below

It does, the remainder is Ti, high ductility TiA of claim 1 statement

I based intermetallic.

Claims

(JP05059469)

1. And so on between the TiAl metal which from the axial crystal are formed
In chemical compound, unit lattice cubic measure of the axial crystal such as the description above 65.2
0 (3) the high ductility TiA which features that it sets under
I based intermetallic.

2. In TiAl based intermetallic constitution amount, 0.

01 atmoic % above, 0.50 atmoic % Ge below is added,
It is, the high ductile TiAl based intermetallic of claim 1 statement.

Claims

(JP05051681)

Claims machine translated from Japanese

1. 36 atomic % above, 60 atomic % Al below

It contains, the TiAl based intermetallic group where the remainder is Ti

Component and 0.01 weight % above, 1 weight % oxygen below

To contain, metallographic structure, TiAl phase I and Ti [3] Al phase

I [To consist of quarter-phase organization which possesses 2], Ti [3] Al phase I [the body of 2]

Integral calculus ratio Vf 1% or more and setting 80% or less special

The high intensity TiAl based intermetallic which is made collection/symbol.

Claims

(JP05051680)

1. Average crystal grain size to be 50 .micro.m or less, containing
The possession oxygen quantity 1.0 weight % features that it is below, high
Strength high *** ductile TiAl based intermetallic.

Claims

(JP05051679)

1. 30 atmoic % above, 60 atmoic % Al below

It contains, the TiAl based intermetallic group where the remainder is Ti

In component, 0.05 atmoic % above, 3 atmoic % In below attachment

Adding chemical combination between the high *** ductile TiAl metal which feature that it does
Thing.

Claims

(JP05051678)

1. 30 atmoic % above, 60 atmoic % Al below

It contains, the TiAl based intermetallic group where the remainder is Ti

Component and 0.05 atmoic % above, 5 atmoic % Ga under containing

Possessing and Ti [3] Al phase I [cubic measure amount ratio Vf of 2] 0.05% from here

The high *** ductility T which features that on and it sets 40% or less

iAl based intermetallic.

Claims

(JP05051677)

1. The TiAl gold which contains Ti and Al
In intergeneric chemical compound constitution amount, 0.05 atmoic % above, 2 atmoic % from here
The high *** ductility TiAl which features that Ge under is added
Type intermetallic.
2. Ti [3] Al phase I [cubic measure amount ratio Vf of 2],
0.05% or more and it set 40% or less, claim 1 statement
High *** ductile TiAl based intermetallic.
3. As for TiAl based intermetallic constitution amount, 35
Atmoic % Above, 60 atmoic % to contain Al below, the remainder T
It is i, claim high *** ductile TiAl system of 1 or 2 statements
Intermetallic.

Claims

(JP07197107)

Claims machine translated from Japanese

1. The Ti powder or the Ti alloy powder it is little

On the one hand (1) and the Al powder or the Al alloy powder little

Also mixing (2) on the one hand, the TiAl based intermetallic

The mixed powder for formation process and that mixed powder which (3) are manufactured

Process temperature T_w is set to $T_w \leq 600 \text{ deg.C}$ making use of (3),It is by doing pressurization fabrication, major diameter D [1] and wall thickness T [1]Bell-shaped ratio T [1] / D [1] is the T [1] / D [1] ≤ 0.2

Process and the aforementioned TiAl metal which obtain the primary intermediate field (5 [1])

When designating the fusion point of between chemical compound as $T_m \text{ deg.C}$, the aforementioned bell-shaped 1In the next intermediate field (5 [1]), sintering temperature T_s $650 \text{ deg.C} \leq T_s \leq$ Administering the sintering processing which is set to $T_m - 20 \text{ deg.C}$, the aforementioned mixed powder

The aforementioned TiAl gold which is formed end (3) by counter diffusion

The bell-shaped secondary intermediate field (5 [2]) consists of intergeneric chemical compound) which profit

In [ru] process and the aforementioned bell-shaped secondary intermediate field (5 [2]) slicing

The process which administers processing and, TiAl which features that it uses

Production method of type intermetallic make ring component.

2. It pushes out the aforementioned pressurization fabrication, ratio R_e R It is extrusion processing which is set to $e \geq 5$, T of claim 1 statement

Production method of iAl based intermetallic make ring component.

3. As for the aforementioned sintering processing, between the aforementioned TiAl metal

When fusion point T_m of chemical compound $1450 \text{ deg.C} \leq T_m \leq 1600 \text{ deg.C}$ Coming and sintering temperature T_s in $900 \text{ deg.C} \leq T_s \leq 1400 \text{ deg.C}$, [ma]It is pressure P [2] the heat which is set to P [2] $\geq 49 \text{ MPa}$ respectively

To be gravitational pressure press processing, in this high-temperature gravitational pressure press processing

From, the aforementioned bell-shaped density ratio R_d is $R_d \geq 85\%$ The secondary intermediate field (5 [2]) is obtained, claim T of 1 or 2 statements

Production method of iAl based intermetallic make ring component.

4. As for ring component piston ring for internal combustion engine

(7) So being, the ring which is obtained by the aforementioned slicing processing

It is agreeable to the condition 3 next intermediate field (5 [3]), and the mouth the machine to which (6) includes formation

Administering device processing, it produces the ring condition 4 next intermediate field (5 [4]),

Next, in the aforementioned ring condition 4 next intermediate field (5 [4]) finishing

Administering, it possesses the hardness which is higher than those 4 next intermediate fields (5 [4])

[ru] surface layer (9) is formed, claim 1,2 or 3 statements

Production method of TiAl based intermetallic make ring component.

5. The Ti powder or the Ti alloy powder it is little

One side (1 [1]) and, the Al powder or the Al alloy powder it is little

Also the [ku] mixing with one side (2 [1]), conversion between the TiAl metal

Process and the mixing which manufacture the mixed powder (3 [1]) for combination thing formation

Making use of the combination powder (3 [1]) process temperature T_w $T_w \leq 600 \text{ deg.C}$ By doing the pressurization fabrication which is set, major diameter D [1][ri] where ratio T of wall thickness T [1] [1] / D [1] is the T [1] / D [1] ≤ 0.2

Process and the aforementioned TiAl gold which obtain the [ngu] condition intermediate field (5 [1])

When designating the fusion point of being attached chemical compound as $T_m \text{ deg.C}$, the aforementioned ring condition centerIn body (5 [1]), sintering temperature T_s $650 \text{ deg.C} \leq T_s \leq T_m -$ Administering the sintering processing which is set to the 20 deg.C , the aforementioned mixed powder (3

[1]) With counter diffusion the aforementioned TiAl based intermetallic raw

Forming the process which is done and, the TiAl gold which features that it uses

Production method of intergeneric chemical compound make ring component.

6. As for the aforementioned pressurization fabrication with powder forging processing [a]

The [ri], with this powder forging processing, density ratio R_d $R_d \geq 60\%$

So the aforementioned ring condition intermediate field (5 [1]) is which is obtained, claim 5 description

Production method of TiAl based intermetallic make ring component of *** .

7. As for the aforementioned sintering processing, density ratio R of ring componentIn order that d is set to $R_d \geq 85\%$, between the aforementioned TiAl metalWhen fusion point T_m of chemical compound $1450 \text{ deg.C} \leq T_m \leq 1600 \text{ deg.C}$ Coming and sintering temperature T_s in $900 \text{ deg.C} \leq T_s \leq 1400 \text{ deg.C}$, [ma]It is pressure P the high-temperature still water which is set to $P \geq 49 \text{ MPa}$ respectively

It is pressure press processing, claim TiAl of 5 or 6 statements

Production method of type intermetallic make ring component.

8. As for ring component piston ring for internal combustion engine

(7 [1]) being, the description above T which is obtained by the aforementioned sintering processing

The ring condition secondary intermediate field which consists of the iAl based intermetallic (5 [2] Administering machining which), is agreeable and includes the formation of the mouth (6 [1]) To produce the ring condition 3 next intermediate field (5 [3]), next, aforementioned [ri] Administering finishing to the [ngu] condition 3 next intermediate field (5 [3]), that 3 The surface layer which possesses the hardness which is higher than the next intermediate field (5 [3]) (9 [1]) it forms, claim Ti of 5,6 or 7 statements
Production method of Al based intermetallic make ring component.

Claims

(JP06049565)

1. Cr and V it is little as a 3rd element

To contain kind, metallographic structure TiAl phase (La) with Ti

[3] Al phase (Lb) with laminating alternately, the stratified organizational territory which becomes

(R [L]) to possess, content A of aforementioned 3rd element 0.5 atoms

$\% \leq A \leq 5$ atomic % to be, in addition the aforementioned stratified organizational territory

(R [L]) cubic measure amount ratio Vf being $V_f \geq 8\%$ feature

With the high intensity high ductile TiAl based intermetallic which is done.

Claims

(JP05070861)

Claims machine translated from Japanese

1. It is constituted from the TiAl based intermetallic,

At the same time I [2] it possesses the stratified organization which laminates with phase and I phase alternately

Calcination to the material which consists of the raw materials powder of mean diameter 500 .micro.m or less

Administering processing, mean diameter below mean diameter of the aforementioned raw materials powder

Obtaining the structural element which has the aforementioned stratified organization which it has feature

That the high *** ductile TiAl based intermetallic make structural element which is done make

Structure method.

Claims

(JP05065558)

Claims machine translated from Japanese

1. The raw materials which include the Ti powder and the Al powder

The TiAl based intermetallic which does calcination processing making use of the powder

In production method, grain size d of the Ti powder [1] 1000.micro.





To set under m , in addition grain size d of the Ti powder [1] the Al powder

Grain size d end [relationship with 2] d [2] $\leq 0.8d$ [was set to 1] densely

That the high intensity high ductile TiAl based intermetallic which is featured

Production method.

Manufacture of high toughness and ductility ti-al intermetallic compound JP05065563

<ul style="list-style-type: none"> • Patent Assignee HONDA MOTOR • Inventor TSUNASHIMA SAKAE FUJIWARA YOSHINARI TOKUNE TOSHIO • International Patent Classification C22C-001/04 C22F-001/00 C22F-001/18 	<ul style="list-style-type: none"> • Publication Information JPH0565563 A 1993-03-19 [JP05065563]     • Priority Details 1991JP-0250283 1991-09-04
<ul style="list-style-type: none"> • Fampat family JPH0565563 A 1993-03-19 [JP05065563] 	

- **Abstract:**

(JP05065563)

PURPOSE: To reduce and control the amt. of Ti(sub 3)Al phases in a lamellar structural part and to obtain a high toughness and ductility Ti-Al intermetallic compound by executing secondary heat treatment at a specified temp. to an intermediate body obtd. by subjecting the stock having isometric system Ti-Al phases to primary heat treatment at a specified temp. CONSTITUTION: When the transformation point in the case of a mixed structure constituted of Ti(sub 3)Al phases a(sub 2) and Ti-Al phases .gamma. is formed by phase transition is defined as T(sub 0), the heat treating temp. T(sub 1) is set to (T(sub 0)-50) deg.C<+T(sub 1)<+T(sub 0) deg.C, and the stock having isometric system Ti-Al phases .gamma.' is subjected to primary heat treatment. Then, an intermediate body provided with a lamellar structural part L in which the Ti(sub 3)Al phases a(sub 2) and the Ti-Al phases .gamma. are alternately deposited is obtd. Next, the heat treating temp. T(sub 2) is set to 1000<+T(sub 2)<+1300 deg.C, and the above intermediate body is subjected to secondary heat treatment. By this method, the volume fractional rate of the Ti(sub 3)Al phases a(sub 2) is controlled to 0.05 to 50%, by which the objective high toughness and ductility Ti-Al intermetallic compound Im can be obtd. COPYRIGHT: (C)1993,JPO&Japio

Claims

(JP05065563)

1. With phase change Ti [3] Al phase I [2] Ti

When causing the mixed phase organization which consists of with Al phase I , the transformation point T

[0] .deg.C When with doing, heat treatment temperature T [1] (T [0] - 50) the .deg.C<=

T [1] <=T [0] .deg.C setting, and so on axial crystal TiAl phase I ' it possesses

By administering primary heat treatment to [ru] material M, Ti [3] Al phase

I [2] and the stratified organizational section which made TiAl phase precipitate I alternately

To produce the intermediate field I which has L, next heat treatment temperature T [2]

1000.deg.C<=T [2] setting to the <=1300.deg.C, the aforementioned intermediate field

By administering secondary heat treatment to I, in the aforementioned stratified organizational section L

Ti which you can put [3] Al phase I [it features that the quantity of 2] is controlled

Production method of [ru] high ductile TiAl based intermetallic.

Claims

(JP05059507)

Claims machine translated from Japanese

1. TiAl phase I and Ti [3] Al phase I [2]

Plural stratified organizational sections L and the phase which were made to precipitate alternately both stratified it is placed next

The pro-eutectoid TiAl phase I which exists between organizational section L ' with the material which it has

Administering heat treatment, the method which produces the TiAl based intermetallic

Being law, Ti [3] Al phase I [2], Ti [3] Al phase I [2]

When phase changing to the mixed phase organization which consists of with TiAl phase I , change

When T [0] .deg.C with doing the condition point, heat treatment temperature T, (T [0] - 5





0) .deg.C=<=T<=T [0] .deg.C setting, pro-eutectoid TiAl phase I '

While controlling coarseness, assuring the enlargement of stratified organizational section L special

The creep resistance TiAl based intermetallic which is made collection/symbol production

Law.

Production of structural member made of tial intermetallic compound JP04210401

<ul style="list-style-type: none"> • Patent Assignee HONDA MOTOR • Inventor FUJIWARA YOSHINARI TOKUNE TOSHIO TSUNASHIMA SAKAE YAGI KAZUHIKO • International Patent Classification B22F-001/00 B22F-003/24 C22C-001/04 	<ul style="list-style-type: none"> • Publication Information JPH04210401 A 1992-07-31 [JP04210401] <div style="text-align: right; margin-top: 5px;">     </div> <ul style="list-style-type: none"> • Priority Details 1990JP-0401811 1990-12-13
<ul style="list-style-type: none"> • Fampat family <div style="display: flex; justify-content: space-between; align-items: flex-start; margin-top: 5px;"> JPH04210401 A 1992-07-31 [JP04210401] </div> 	

- **Abstract:**
(JP04210401)
PURPOSE: To produce a high strength structural member made of TiAl intermetallic compound at low sintering temp. by mixing, by agitation, powdered Ti and powdered Al together with powdered TiH(sub 2), compacting the resulting composite powder, exerting sintering treatment, and applying dehydrogenation treatment to the resulting sintered compact. CONSTITUTION: Powdered Ti and powdered Al are mixed by means agitation in the presence of powdered TiH(sub 2) by the use of a high energy ball mill, etc., by which a composite powder consisting of Ti, Al, and TiH(sub 2) and excellent in dispersibility is formed. Subsequently, a green compact is formed by using this composite powder. This green compact is sintered at about 800-1200 deg.C by means of hot isostatic pressing. The resulting sintered compact is subjected to dehydrogenation treatment. By this method, the structural member made of TiAl intermetallic compound having high density and high strength can be obtained. COPYRIGHT: (C)1992,JPO&Japio

Claims

(JP04210401)

JP40181190 1990-12-13 [1990JP-0401811]